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Europäisches Patentamt
European Patent Office
Office européen des brevets



(11) Publication number:

0 425 740 A1

(12)

EUROPEAN PATENT APPLICATION(21) Application number: **89311262.3**(51) Int. Cl.⁵: **C07C 15/08, C07C 7/13**(22) Date of filing: **31.10.89**(43) Date of publication of application:
08.05.91 Bulletin 91/19(84) Designated Contracting States:
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London WC1V 6DE(GB)(54) **Adsorptive separation of para-xylene.**

(57) Para-xylene is separated from a feed mixture of C₈ isomers of xylene and C₉ aromatics by contacting the para-xylene-containing feed mixture with a crystalline aluminosilicate zeolite, e.g. an X or Y zeolite adsorbent having Group IA or IIA cations, e.g. barium and/or potassium, at exchangeable cationic sites. The para-xylene is selectively adsorbed onto the adsorbent. The non-adsorbed feed is then removed from the adsorbent and the para-xylene recovered from the resulting rich adsorbent by desorption with a desorbent comprising 1,2,3,4-tetrahydronaphthalene or an alkyl or dialkyl derivative of 1,2,3,4-tetrahydronaphthalene or mixtures thereof. The majority of the C₉ aromatics and the xylene isomers are typically recovered in the raffinate and can be separated from the desorbent by fractionation of the raffinate and the recovered desorbent recycled to the process.

EP 0 425 740 A1

ADSORPTIVE SEPARATION OF PARA-XYLENE

FIELD OF THE INVENTION

5 The field of art to which the claimed invention pertains is adsorptive hydrocarbon separation. More specifically, the invention relates to a process for separating para-xylene from a feed mixture comprising at least one other xylene isomer and C₉ aromatic hydrocarbons, which process employs a zeolitic adsorbent and a tetralin desorbent. It is particularly advantageous in a process in which the feed contains large amounts of C₉ aromatic hydrocarbons, which are known to cause problems in prior adsorptive separation processes of this type.

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BACKGROUND OF THE INVENTION

15 In numerous processes described in the patent literature, for example U.S. Patents 3,626,020 to Neuzil, 3,663,638 to Neuzil, 3,665,046 to deRosset, 3,668,266 to Chen et al., 3,686,342 to Neuzil et al., 3,700,744 to Berger et al., 3,734,974 to Neuzil, 3,894,109 to Rosback, 3,997,620 to Neuzil and 4,014,949 to Hedge, particular zeolitic adsorbents are used to separate the para isomer of dialkyl substituted monocyclic aromatics from the other isomers, particularly para-xylene from other xylene isomers. Many of the above
20 patents teach the use of benzene, toluene, or p-diethylbenzene as the desorbent. P-diethylbenzene (p-DEB) has become a commercial standard for this separation. However, p-DEB is a "heavy" desorbent (higher boiling than p-xylene) which causes problems in a process for adsorptive separation of p-xylene when the feed mixtures also contain C₉ aromatics because the boiling point of p-DEB is too close to the boiling point of C₉ aromatics in the feed and thus separation by simple fractionation is difficult. Because the C₉
25 aromatics if allowed in the feed to the adsorptive separation are difficult to separate from p-DEB by simple fractionation, the C₉ aromatics would gradually build up in the desorbent, which must be recycled for economic reasons. In the prior art process for recovering p-xylene from feed mixtures containing isomers using para-diethylbenzene as the desorbent, therefore, it has been necessary to reduce C₉ aromatics in the feed to below about 0.1 wt.% prior to the adsorptive separation of p-xylenes. This is usually done by
30 distillation in a so-called xylene splitter column. Of course, substantial costs associated with this practice, such as capital costs of the xylene splitter and utilities necessary to achieve substantially complete removal of the C₉ aromatics, could be reduced greatly or eliminated if it were not necessary to first remove C₉ aromatics. Thus, while U.S. Patent 3,686,342, supra, mentions tetralin as a possible heavy desorbent for the para-xylene separation process, that reference clearly states that p-DEB is the best desorbent for the
35 separation and, further, does not address the problem that the preferred desorbents may have in separating feeds containing C₉ aromatics. Therefore, a higher boiling point material, that meets the selectivity requirements for desorbents and can be separated from C₉ aromatics, has been long sought and is still desirable.

It is also known that crystalline aluminosilicates or zeolites are used in adsorption separations of various
40 mixtures in the form of agglomerates having high physical strength and attrition resistance. Methods for forming the crystalline powders into such agglomerates include the addition of an inorganic binder, generally a clay comprising a silicon dioxide and aluminum oxide, to the high purity zeolite powder in wet mixture. The blended clay zeolite mixture is extruded into cylindrical type pellets or formed into beads which are subsequently calcined in order to convert the clay to an amorphous binder of considerable
45 mechanical strength. As binders, clays of the kaolin type, water permeable organic polymers or silica are generally used.

The invention herein can be practiced in fixed or moving adsorbent bed systems, but the preferred system for this separation is a countercurrent simulated moving bed system, such as described in Broughton U.S. Patent 2,985,589, incorporated herein by reference. Cyclic advancement of the input and
50 output streams can be accomplished by a manifolding system, which are also known, e.g., by rotary disc valves shown in U.S. Patents 3,040,777 and 3,422,848. Equipment utilizing these principles are familiar, in sizes ranging from pilot plant scale (deRosset U.S. Patent 3,706,812) to commercial scale in flow rates from a few cc per hour to many thousands of gallons per hour.

The invention may also be practiced in a cocurrent, pulsed batch process, like that described in U.S. Patent 4,159,284 or in a cocurrent, pulsed continuous process, like that in Gerhold Patents 4,402,832 and

4,478,721.

Also, in some cases illustrated herein, it is necessary to remove three effluent streams from the adsorptive separation step in order to obtain a desired product intermediate in adsorption strength from an extract and a raffinate stream. This intermediate stream can be termed a second raffinate stream, as in U.S. Patent 4,313,015 or a second extract stream, as in U.S. Patent 3,723,302, both incorporated herein by reference. This case pertains when a contaminating component in the feed, such as p-ethyltoluene, is more strongly adsorbed than the desired product, p-xylene. It is not always necessary to remove p-ethyltoluene from p-xylene, e.g., where terephthalic acid is the final product of the oxidation of p-xylene, since oxidation of p-ethyltoluene results in the same product. However, if it is desired to keep the concentration of the contaminating component in the product as low as possible, a first extract is taken off, high in concentration of the desired component and lower in the contaminating product followed by a second extract, withdrawn at a point between the desorbent inlet and the first extract point, containing a high concentration of the contaminant and a lower concentration of the desired product. It is not necessary, however, to use a second desorbent, if the desorbent is able to first desorb the lightly held product and then desorb the remaining more strongly held contaminants, as disclosed in the aforementioned 3,723,302 patent. If the contaminating component in high concentrations and purity is desired, this can be achieved by withdrawing a second extract in the cocurrent pulsed batch process mentioned above.

The functions and properties of adsorbents and desorbents in the chromatographic separation of liquid components are well-known, but for reference thereto, Zinnen et al. U.S. Patent 4,642,397 is incorporated herein.

A process employing a zeolite adsorbent for the separation of p-xylene from its isomers using a desorbent which is a substantial improvement in a process for separating xylene isomers where the feed mixture also contains C₉ aromatic impurities has now been discovered.

SUMMARY OF THE INVENTION

In brief summary, the invention is a chromatographic process for separating p-xylene from a feed mixture comprising p-xylene, C₉ aromatic hydrocarbons and one or more additional xylene isomers (including ethylbenzene) comprising contacting said feed mixture with an X- or Y-type zeolite exchanged with Group IA or IIA metal ions at exchangeable cationic sites to effect the selective adsorption of said p-xylene and produce a raffinate comprising C₉ aromatic hydrocarbons and the non-paraxylene isomers, including ethylbenzene. P-xylene is thereafter recovered by contacting the resulting p-xylene rich adsorbent with a desorbent comprising 1,2,3,4-tetrahydronaphthalene (tetralin) or an alkyl, or dialkyl derivative of tetralin and mixtures thereof. These desorbents are all higher boiling (tetralin-b.p. 206°C) than the C₉ aromatics, making it possible to separate the C₉ aromatics from the desorbent by simple fractionation so that the desorbent can be reused in the process without building up C₉ aromatics in the recycled desorbent.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a chromatographic representation of the separation of p-xylene from a mixture of xylene isomers and C₉ aromatics with a K-exchanged Y zeolite and a desorbent comprising a 30/70 mixture of tetralin and n-heptane.

Figure 2 is similar to Figure 1 except that the adsorbent is BaX.

Figure 3 is similar to Figure 1 except that the desorbent diluent is n-octane and shows the chromatographic separation of para-ethyl toluene and para-xylene from other C₈ and C₉ aromatics.

Figure 4 is similar to Figure 2 except that the desorbent diluent is n-octane and shows the separation of p-xylene from p-ethyltoluene and other isomers of xylene.

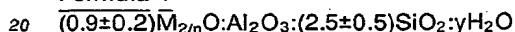
In the figures, numerals are used to indicate the component lines in the graph of relative concentrations vs. retention volume (ml.) as follows: the tracer 1; mesitylene 2; m-xylene 3; n-propylbenzene 4; o-xylene 5; 1,2,3-trimethylbenzene 6; ethylbenzene 7; 1,2,4-trimethylbenzene 8; cumene 9; p-xylene 10 and p-ethyltoluene 11.

DETAILED DESCRIPTION OF THE INVENTION

Adsorbents to be used in the process of this invention comprise specific crystalline aluminosilicate zeolites or molecular sieves, namely X and Y zeolites. The zeolites have known cage structures in which the alumina and silica tetrahedra are intimately connected in an open three-dimensional network to form cage-like structures with window-like pores. The tetrahedra are cross-linked by the sharing of oxygen atoms with spaces between the tetrahedra occupied by water molecules prior to partial or total dehydration of this zeolite. The dehydration of the zeolite results in crystals interlaced with cells having molecular dimensions and thus, the crystalline aluminosilicates are often referred to as "molecular sieves" when the separation which they effect is dependent essentially upon differences between the sizes of the feed molecules as, for instance, when smaller normal paraffin molecules are separated from larger isoparaffin molecules by using a particular molecular sieve. In the process of this invention, however, the term "molecular sieves", although widely used, is not strictly suitable since the separation of specific aromatic isomers is apparently dependent on differences in electrochemical attraction of the different isomers and the adsorbent rather than on pure physical size differences in the isomer molecules.

In hydrated form, the crystalline aluminosilicates encompass type X zeolites which are represented by Formula 1 below in terms of moles of oxides:

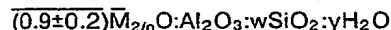
Formula 1



where "M" is a cation having a valence of not more than 3 which balances the electrovalence of the alumina tetrahedra and is generally referred to as an exchangeable cationic site, "n" represents the valence of the cation, and "y", which represents the moles of water, is a value up to about 9 depending upon the identity of "M" and the degree of hydration of the crystal. As noted from Formula 1, the SiO_2/Al_2O_3 mole ratio is 2.5 ± 0.5 . The cation "M" may be monovalent, divalent or trivalent cations or mixtures thereof.

The type Y structured zeolite, in the hydrated or partially hydrated form, can be similarly represented in terms of moles of oxides as in Formula 2 below:

Formula 2



where "M", "n" and "y" are the same as above and "w" is a value greater than about 3 up to about 6. The SiO_2/Al_2O_3 mole ratio for type Y structured zeolites can thus be from about 3 to about 6. For both zeolites, the cation "M" may be one or more of a variety of cations but, as the zeolites are initially prepared, the cation "M" is also usually predominately sodium. The type Y zeolite containing predominately sodium cations at the exchangeable cationic sites is, therefore, referred to as a sodium-exchanged type-Y, or NaY, zeolite. Depending upon the purity of the reactants used to make the zeolite, other cations mentioned above may be present, however, as impurities.

The zeolites useful in the invention are typical as described above. However, the exchange of the cation of the as-manufactured zeolite by ions from Group IA or IIA, e.g., barium or potassium or mixtures thereof, is necessary to achieve the separation.

Typically, adsorbents used in separative processes contain the crystalline material dispersed in an amorphous, inorganic matrix or binder, having channels and cavities therein which enable liquid access to the crystalline material. Silica, alumina, clay or mixtures thereof are typical of such inorganic matrix materials. The binder aids in forming or agglomerating the crystalline particles which otherwise would comprise a fine powder. The adsorbent may thus be in the form of particles such as extrudates, aggregates, tablets, macrospheres or granules having a desired particle range, preferably from about 16 to about 60 mesh (Standard U.S. Mesh) (250 to 1190 microns).

Feed mixtures which can be utilized in the process of this invention will comprise para-xylene, at least one other C_8 aromatic isomer, and may also contain one or more C_9 aromatics as impurities. Mixtures containing substantial quantities of para-xylene and other C_8 aromatic isomers and C_9 aromatics generally are produced by reforming and isomerization processes, processes which are well known to the refining and petrochemical arts. Many of the C_9 aromatics have boiling points in the range of 160-170°C and cannot be easily removed by distillation from the standard desorbent, p-diethylbenzene. In the current process, therefore, the C_9 's are usually removed from the feed by distillation before the adsorptive separation step and consequent contact with the normal desorbent. A desorbent has now been discovered which can be easily separated from the C_9 aromatics by fractionation after the adsorption step and does not thus require the large column and quantity of utilities to pretreat the feed, resulting in substantial cost savings.

Reforming processes can provide feed mixtures for the process of this invention. In reforming processes, a naphtha feed is contacted with a platinum-halogen-containing catalyst at severities selected to

produce an effluent containing C_8 aromatic isomers. Generally, the reformat is then fractionated to concentrate the C_8 aromatic isomers in a C_8 fraction which will contain the C_8 aromatic isomers as well as C_8 nonaromatics and C_9 aromatics. Feed mixtures for the process of this invention may also be obtained from isomerization and transalkylation processes. Xylene mixtures which are deficient in one or more isomers can be isomerized, at isomerization conditions, to produce an effluent containing C_8 aromatic isomers, e.g., enriched in p-xylene, as well as C_8 nonaromatics and C_9 aromatics. The C_9 aromatic content of isomerized xylene isomers can be as much as 1-2 wt.% depending on isomerization conditions. Likewise, transalkylation of mixtures of C_7 and C_9 aromatics produces xylene isomers. In all of these catalytic routes, the xylene splitter column must be employed to remove C_9 aromatics from C_8 aromatics before conventional adsorptive xylene separation methods can be employed. Thus, the feed mixtures to the process of this invention can contain quantities of C_9 aromatics and may also contain quantities of straight or branched chain paraffins, cycloparaffins, or olefinic material. It is preferable to have these quantities at a minimum amount in order to prevent contamination of products from this process by materials which are not selectively adsorbed or separated by the adsorbent. Preferably, the above-mentioned contaminants should be less than about 20% of the volume of the feed mixture passed into the process.

To separate the para-xylene from a feed mixture containing para-xylene, at least one other C_8 aromatic and C_9 aromatics, the mixture is contacted with the adsorbent at adsorption conditions and the para-xylene (and para-ethyltoluene, if present) is more selectively adsorbed and retained by the adsorbent while the other components are relatively unadsorbed and are removed from the interstitial void spaces between the particles of adsorbent and from the surface of the adsorbent. The adsorbent containing the more selectively adsorbed para-xylene is referred to as a "rich" adsorbent-rich in the more selectively adsorbed para-xylene. The para-xylene is then recovered from the rich adsorbent by contacting the rich adsorbent with the instant tetralin or tetralin derivative desorbent material at desorption conditions.

In this process, which employs zeolitic adsorbents and which is generally operated continuously at substantially constant pressures and temperatures to ensure liquid phase, the desorbent material relied upon must be judiciously selected to satisfy several criteria. First, the desorbent material should displace an extract component from the adsorbent with reasonable mass flow rates without itself being so strongly adsorbed as to unduly prevent the extract component from displacing the desorbent material in a following adsorption cycle. Secondly, the desorbent material must be compatible with the particular adsorbent and the particular feed mixture. More specifically, they must not reduce or destroy the critical selectivity of the adsorbent for an extract component with respect to the raffinate component or react chemically with the feed components. Desorbent materials should additionally be easily separable from the feed mixture that is passed into the process. Both the raffinate components and the extract components are typically removed from the adsorbent in admixture with desorbent material and without a method of separating at least a portion of desorbent material, the purity of the extract product and the raffinate product would not be very high nor would the desorbent material be available for reuse in the process. It is, therefore, contemplated that the desorbent material used in this process will have a substantially different average boiling point than that of the feed mixture or any of its components, i.e., more than about 5°C difference, to allow separation of at least a portion of the desorbent material from feed components in the extract and raffinate streams by simple fractional distillation, thereby permitting reuse of desorbent material in the process.

Finally, desorbent materials should be readily available and reasonable in cost. However, a suitable desorbent or desorbents for a particular separation with specific adsorbent are not always predictable. In the preferred isothermal, isobaric, liquid-phase operation of the process of this invention, when the feed material to the separation process contains more than about 0.1 wt.% C_9 aromatics, it has been found that a desorbent material comprising tetralin or alkyl or dialkyl derivatives of tetralin or mixtures thereof will desorb the extract from the adsorbent and can be separated from the C_9 aromatics containing raffinate by distillation.

Suitable alkyl-substituted derivatives of tetralin include methyl tetralin, ethyl tetralin, propyl tetralin, isopropyltetralin, etc. Suitable dialkyl-substituted derivatives of tetralin include methyl-ethyl tetralin, dimethyl tetralin, diethyltetralin, etc. Mixtures of tetralin with one or more of these derivatives as well as mixtures of these derivatives also may be used with good results. In addition to tetralin, methyl tetralin and 2,6-dimethyl tetralin are preferred as desorbents in this process. All position isomers and mixtures are intended to be included when any tetralin derivative is referred to herein.

Adsorption conditions will include a temperature range of from about 20 to about 250°C with about 60 to about 200°C being more preferred and a pressure just sufficient to maintain liquid phase, which may be from about atmospheric to 600 psig. Desorption conditions will include the same range of temperatures and pressure as used for adsorption conditions.

A dynamic testing apparatus is employed to test various adsorbents and desorbent material with a

particular feed mixture to measure the adsorbent characteristics of adsorptive capacity and exchange rate. The apparatus consists of a helical adsorbent chamber of approximately 70 cc volume having inlet and outlet portions at opposite ends of the chamber. The chamber is contained within a temperature control means and, in addition, pressure control equipment is used to operate the chamber at a constant
 5 predetermined pressure. Quantitative and qualitative equipment, such as refractometers, polarimeters, chromatographs, etc., can be attached to the outlet line of the chamber and used to analyze, "on-stream", the effluent stream leaving the adsorbent chamber.

A pulse test, performed using this apparatus and the following general procedure, is used to determine data, e.g., selectivities, for various adsorbent systems. The adsorbent is filled to equilibrium with a particular
 10 desorbent by passing the desorbent material through the adsorbent chamber. At a convenient time, a pulse of feed containing known concentrations of a tracer and of a particular extract component or of a raffinate component, or both, all diluted in desorbent material is injected for a duration of several minutes. Desorbent flow is resumed, and the tracer and the extract and raffinate components are eluted as in a liquid-solid chromatographic operation. The effluent can be analyzed by on-stream chromatographic equipment and
 15 traces of the envelopes of corresponding component peaks developed. Alternatively, effluent samples can be collected periodically and later analyzed separately by gas chromatography.

From information derived from the test, adsorbent performance can be rated in terms of void volume, retention volume for an extract or a raffinate component, and the rate of desorption of an extract component from the adsorbent and selectivity. Void volume is the non-selective volume of the adsorbent, which is
 20 expressed by the amount of desorbent pumped during the interval from initial flow to the center of the peak envelope of the tracer. The net retention volume (net) of an extract or a raffinate component may be characterized by the distance between the center of the peak envelope (gross retention volume) of the extract or raffinate component and the center of the peak envelope (void volume) of the tracer component or some other known reference point. It is expressed in terms of the volume in cubic centimeters of
 25 desorbent material pumped during this time interval represented by the distance between the peak envelopes. The rate of exchange or desorption rate of an extract component with the desorbent material can generally be characterized by the width of the peak envelopes at half intensity. The narrower the peak width, the faster the desorption rate. The desorption rate can also be characterized by the distance between the center of the tracer peak envelope and the disappearance of an extract component which has just been
 30 desorbed. This distance is again the volume of desorbent material pumped during this time interval. Selectivity, β , is determined by the ratio of the net retention volumes of the more strongly adsorbed component to each of the other components.

The following non-limiting examples are presented to illustrate the process of the present invention and are not intended to unduly restrict the scope of the claims attached hereto.

EXAMPLE I

In this experiment, a pulse test, using the apparatus as described above, was performed to evaluate the
 40 ability of the present invention to separate para-xylene (b.p. 138°C) from the other xylene isomers and ethylbenzene (b.p.'s. from 136-145°C) and from C₉ aromatics. The adsorbent used was a Y faujasite exchanged with potassium, dried to yield a loss upon ignition (LOI) of 1.26% at 900°C combined with 15 wt.% of an amorphous clay binder.

For each pulse test, the column was maintained at a temperature of 150°C and at a pressure of 165
 45 psig (1240 kPa) so as to maintain liquid-phase operations. Gas chromatographic analysis equipment was attached to the column effluent stream in order to determine the composition of the effluent material at given time intervals. The feed mixture employed for each test was 5 cc of a mixture containing 0.45 cc each of the xylene isomers and ethylbenzene and each of the following C₉ aromatics: cumene, n-propylbenzene, p-ethyltoluene, mesitylene, 1,2,4-trimethylbenzene and 1,2,3-trimethylbenzene. Normal non-
 50 ane (0.45 cc) was used as a tracer and 4.95 cc desorbent material was added to the feed. The desorbent material comprised 30 vol.% tetralin with the remainder being n-C₇ paraffin. The operations taking place for the test were as follows: The desorbent material was run continuously at a rate of about 1.44 cc per minute. At some convenient time interval, the desorbent was stopped and the feed mixture was run for a 3.47 minute interval. The desorbent stream was then resumed and continued to pass into the adsorbent column
 55 until all of the feed aromatics had been eluted from the column as determined by chromatographic analysis of the effluent material leaving the adsorption column.

The results of the tests shown in Table 1 and the chromatographic tracing of Figure 1 illustrate the invention. The table lists the gross retention volume (GRV) and net retention volume (NRV) for each

component of the feed and the selectivity, β , for each component with respect to the reference, p-xylene.

TABLE 1

Component	Figure 1 Reference No.	Gross Retention Volume(ml)	Net Retention Volume(ml)	Selectivity β	Boiling Point (°C)
n-Nonane	1	47.7	0.0	(Tracer)	
Ethylbenzene	7	59.8	12.1	1.43	136
p-Xylene	10	65.0	17.3	1.00(Ref.)	138
Cumene	9	63.3	15.7	1.11	153
o-Xylene	5	55.6	7.9	2.18	144
n-Propylbenzene	4	53.9	6.3	2.77	159
p-Ethyltoluene	11	75.2	27.5	0.63	162
Mesitylene	2	53.6	5.9	2.92	163
1,2,4-Trimethylbenzene	8	62.9	15.3	1.13	168
1,2,3-Trimethylbenzene	6	60.3	12.6	1.37	175
m-Xylene	3	53.0	5.3	3.26	139

EXAMPLE II

Example I was repeated except that the zeolite was a barium-exchanged X-type zeolite dried to yield an LOI of 4.7% at 900°C. The results are shown in Figure 2 and the following Table 2.

TABLE 2

Component	Figure 2 Reference No.	Gross Retention Volume(ml)	Net Retention Volume(ml)	Selectivity β
n-Nonane	1	42.1	0.0	(Tracer)
Ethylbenzene	7	53.5	11.3	1.86
p-Xylene	10	63.2	21.1	1.00(Ref.)
Cumene	9	52.6	10.5	2.01
o-Xylene	5	50.1	8.0	2.64
n-Propylbenzene	4	50.9	8.8	2.40
p-Ethyltoluene	11	65.4	23.3	0.90
Mesitylene	2	45.4	3.2	6.50
1,2,4-Trimethylbenzene	8	53.4	11.2	1.88
1,2,3-Trimethylbenzene	6	50.9	8.8	2.40
m-Xylene	3	49.2	7.1	2.97

EXAMPLE III

Another pulse test was run under the same conditions and with the same materials as Example I, except that the desorbent was diluted with n-octane instead of n-heptane and the tracer was n-C₆ instead of n-C₉. The feed was 2 cc of a solution containing 0.5 g each of the following materials: n-C₆; ethylbenzene, p-xylene, m-xylene, o-xylene and p-ethyltoluene. The adsorbent was dried to yield an LOI of 0.64%. The results are shown in Figure 3 and the following Table 3.

TABLE 3

Component	Figure 3 Reference No.	Gross Retention Volume(ml)	Net Retention Volume(ml)	Peak Width at Half Height(ml)	Selectivity β
n-C ₆	1	43.8	0	8.3	Tracer
Ethylbenzene	7	56.9	13.1	12.3	1.50
p-Xylene	10	63.5	19.7	11	(Ref.)
m-Xylene	3	49.1	5.3	11.2	3.72
O-Xylene	5	51.8	8	12.6	2.46
p-Ethyltoluene	11	78	34.2	16.9	0.58

EXAMPLE IV

The pulse test of Example III was repeated except that the adsorbent was a barium-exchanged X-type zeolite dried to yield an LOI of 2% at 900°C. The results are shown in Figure 4 and the following Table 4.

TABLE 4

Component	Figure 4 Reference No.	Gross Retention Volume(ml)	Net Retention Volume(ml)	Peak Width At Half Height(ml)	Selectivity β
n-Hexane	1	39.4	0	9.9	Tracer
Ethylbenzene	7	49.1	9.7	18.5	2.84
p-Xylene	10	66.9	27.5	18.8	Refer.
m-Xylene	3	52.1	12.7	22.1	2.17
o-Xylene	5	49.4	10	19	2.75
p-Ethyltoluene	11	58.4	19	26.4	1.45

EXAMPLE V

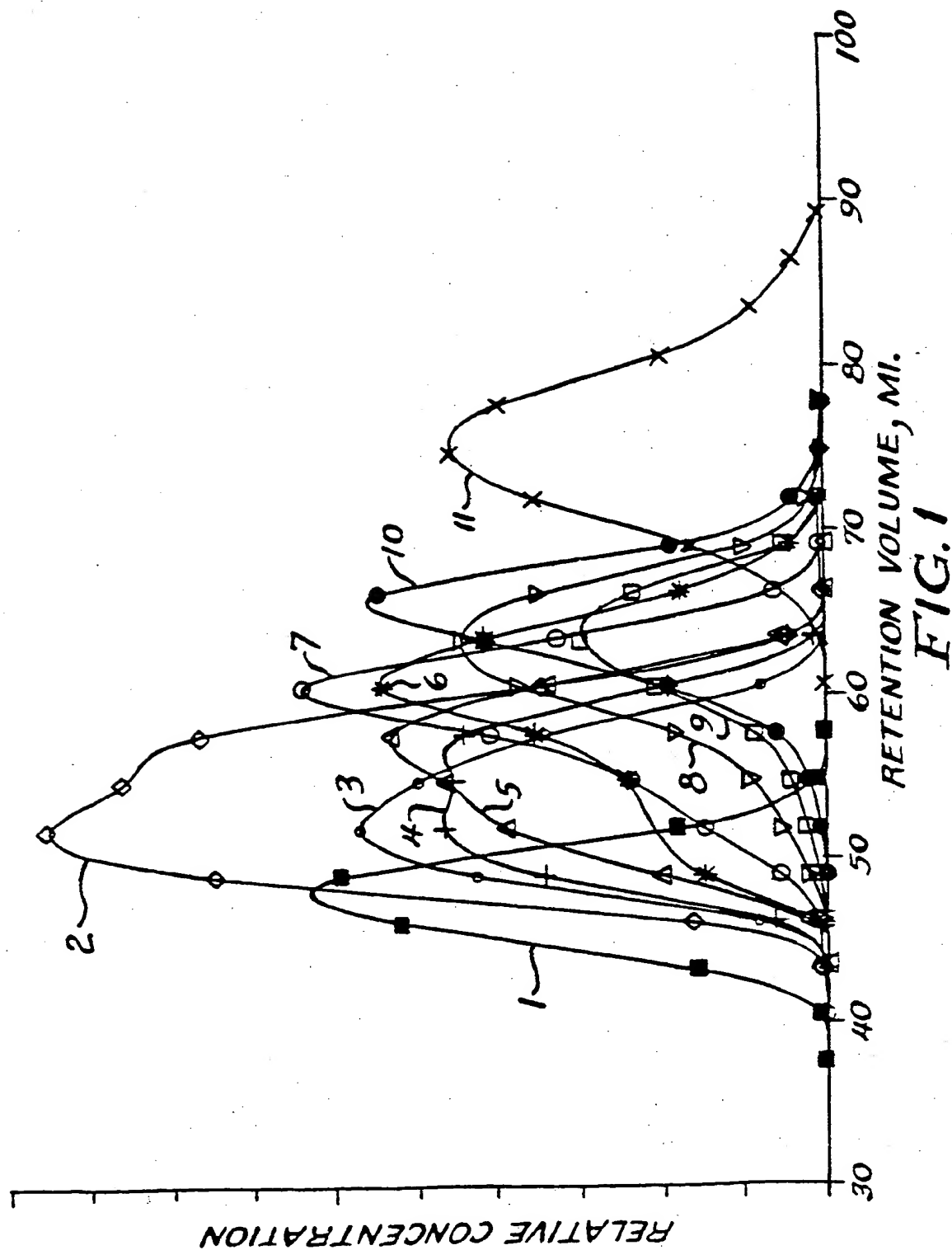
Example II was repeated except that the desorbent was a 30/70 wt.% mixture of methyl tetralin and heptane, the LOI of the adsorbent, BaX, was 4.02% at 500°C and the column flow rate was 1.23 cc/min. The methyl tetralin was a 35/65 wt.% mixture of the two possible isomers, 5-methyl tetralin and 6-methyl tetralin. The results are shown in the following Table 5, indicating improved selectivity for p-xylene over ethylbenzene and slightly better selectivity over p-ethyl toluene.

TABLE 5

Component	Gross Retention Volume(ml)	Net Retention Volume(ml)	Selectivity β
n-C ₉	39.7	0.0	(Tracer)
Ethylbenzene	52.5	12.8	2.20
p-Xylene	67.9	28.2	1.00(Ref.)
m-Xylene	47.3	7.6	3.71
o-Xylene	46.8	7.1	3.97
Cumene	51.1	11.3	2.50
n-Propylbenzene	47.7	7.9	3.57
p-Ethyltoluene	64.6	24.9	1.13
Mesitylene	43.2	3.5	8.06
1,2,4-Trimethylbenzene	48.9	9.1	3.10
1,2,3-Trimethylbenzene	46.1	6.3	4.48
m-Xylene	49.2	7.1	3.97

Claims

1. A process for separating p-xylene from a mixture comprising C₉ aromatic hydrocarbon(s), p-xylene and at least one other xylene isomer, which process comprises the steps of: contacting the mixture with an adsorbent comprising a crystalline aluminosilicate zeolite containing a Group IA or IIA metal ion at exchangeable cationic sites at adsorption conditions to effect the selective adsorption of the p-xylene by the adsorbent and to produce a raffinate stream comprising less strongly adsorbed C₉ aromatic hydrocarbon(s) and the other xylene isomer(s) and thereafter contacting the resulting p-xylene-containing adsorbent with a desorbent at desorption conditions and recovering the p-xylene by desorption from the adsorbent as a first extract stream, characterised in that the desorbent comprises 1,2,3,4-tetrahydronaphthalene, or an alkyl or dialkyl derivative thereof or mixtures thereof.
2. A process as claimed in claim 1, characterised in that the desorbent comprises tetralin or methyl tetralin or a mixture thereof.
3. A process as claimed in claim 1 or 2, characterised in that the adsorbent is selected from type X and type Y zeolites.
4. A process as claimed in any of claims 1 to 3, characterised in that a second extract stream comprising more strongly held C₉ aromatic hydrocarbon(s) is recovered in the desorption step after the first extract stream.
5. A process as claimed in any of claims 1 to 4, characterised in that the zeolite is exchanged with potassium or barium, or a mixture thereof, at exchangeable cationic sites.
6. A process as claimed in any of claims 1 to 5, characterised in that the raffinate stream is fractionated to separately recover C₉ aromatic hydrocarbon(s), the desorbent material substantially free of C₉ aromatic hydrocarbons and the other xylene isomer(s), and the resulting recovered desorbent material is recycled to the desorption step of the process.
7. A process as claimed in any of claims 1 to 6, characterised in that the feed mixture contains more than 0.1 wt% but less than 20% by volume of C₉ aromatic hydrocarbons.
8. A process as claimed in any of claims 1 to 7, characterised in that the desorbent contains up to 90%, preferably up to 80%, of a diluent, preferably an n- or iso-paraffin of 4-14 carbon atoms, preferably 6-9 carbon atoms.
9. A process as claimed in any of claims 1 to 8, characterised in that the process is practiced in a cocurrent, pulsed system.
10. A process as claimed in any of claims 1 to 8, characterised in that the process is practiced in a countercurrent, simulated moving bed system.



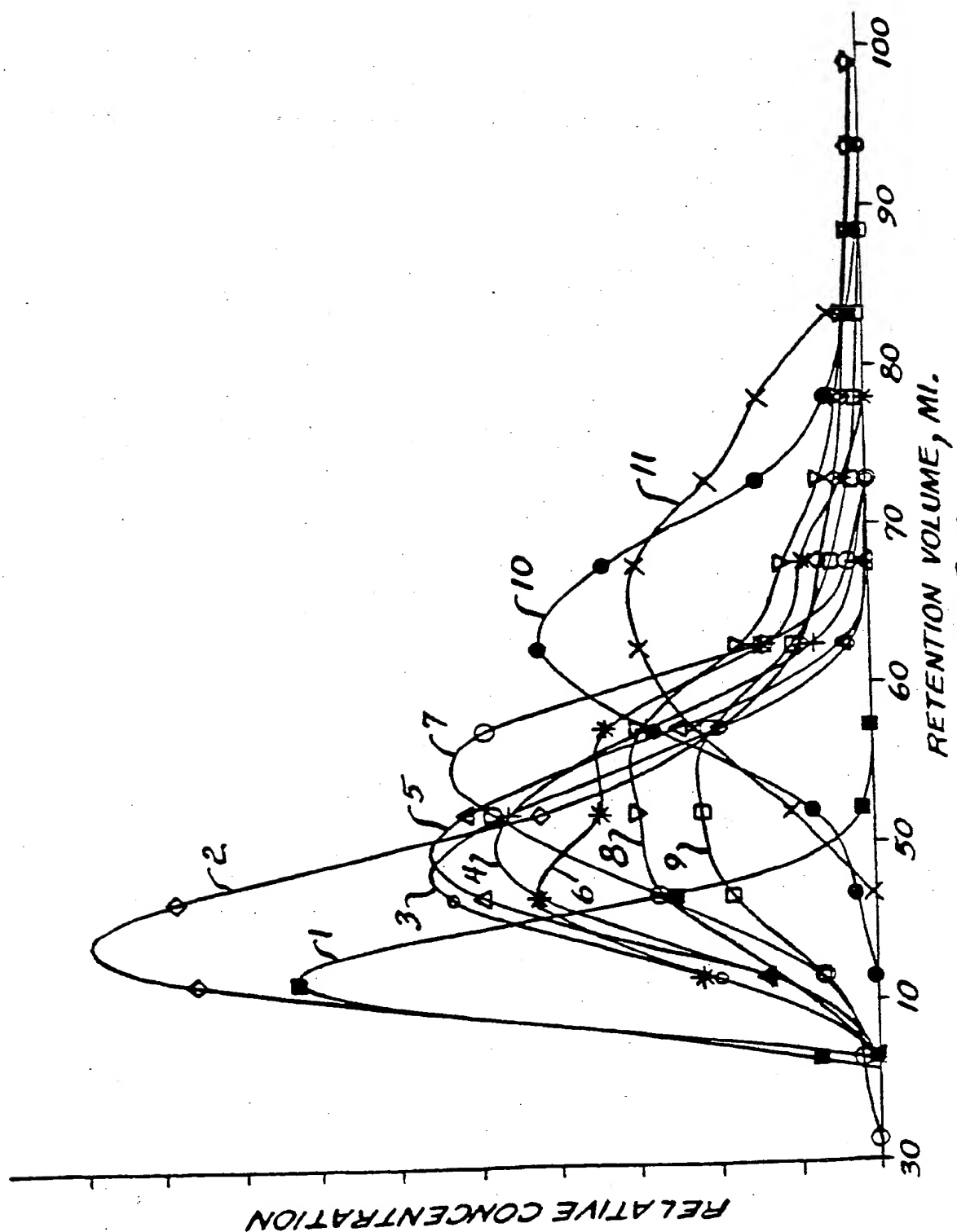
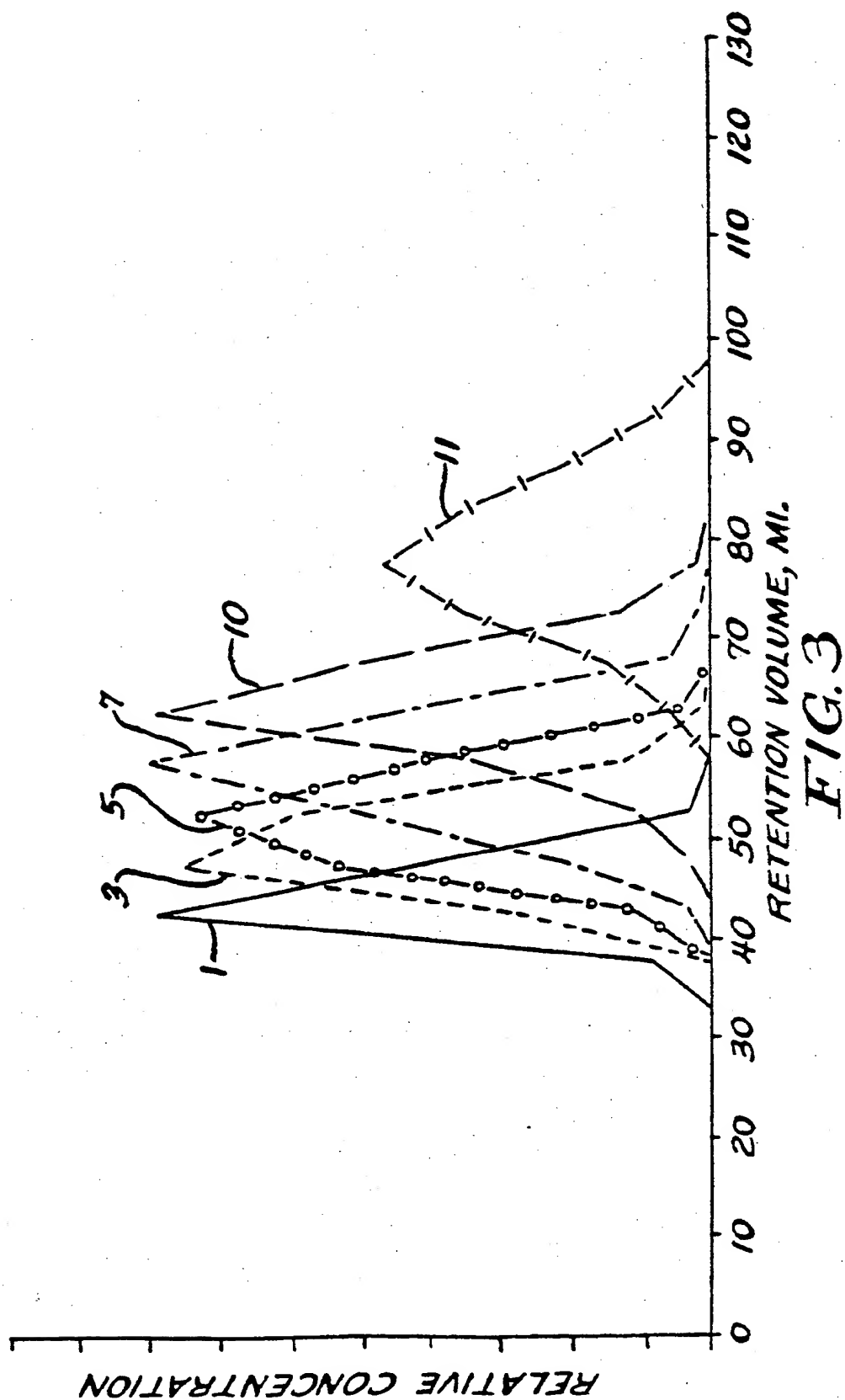


FIG.2



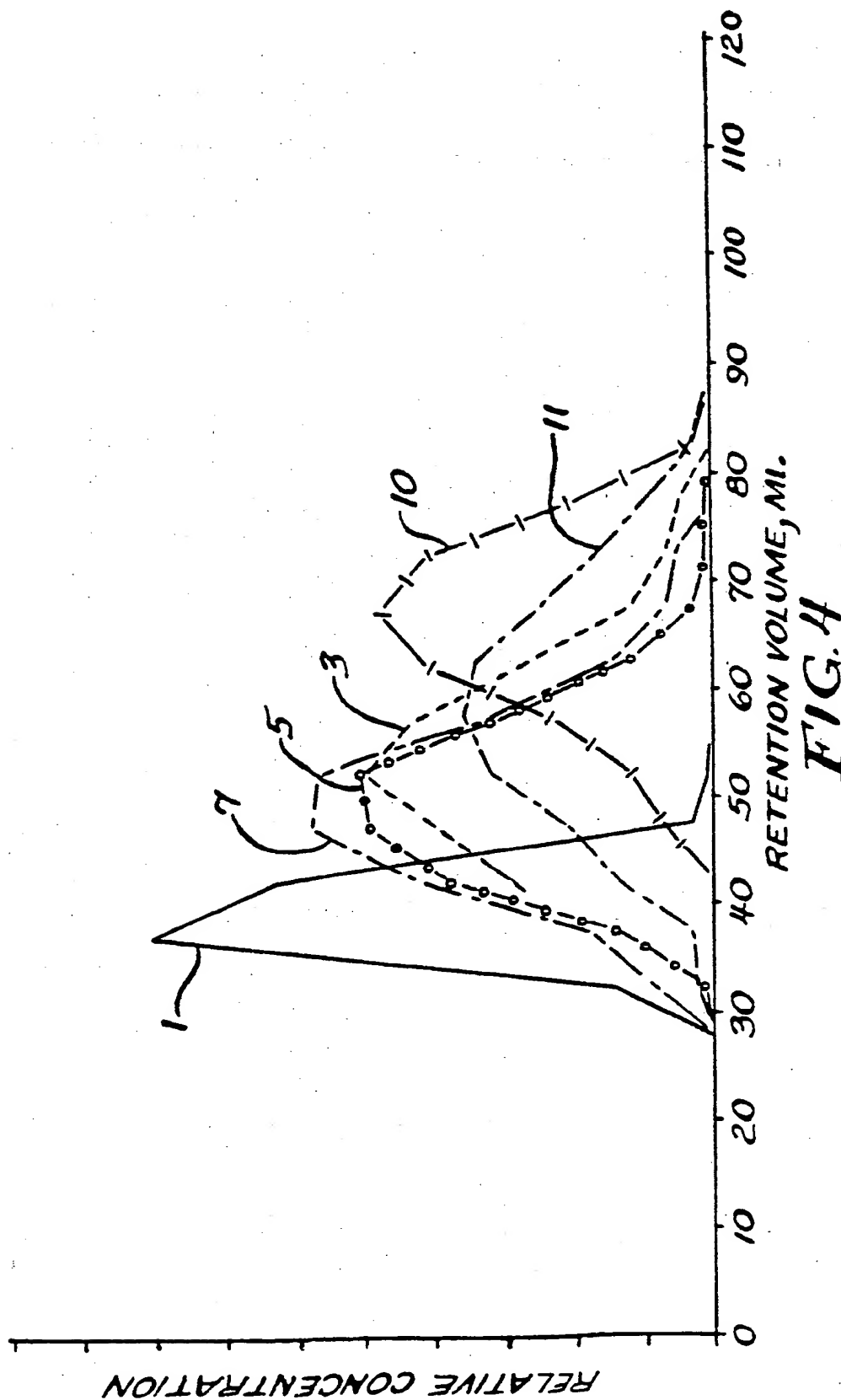


FIG. 4



European Patent
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EUROPEAN SEARCH REPORT

Application Number

EP 89 31 1262

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
X	US-A-4 864 069 (ZINNEN) * Claims *	3-7	C 07 C 15/08 C 07 C 7/13
D,X	US-A-3 686 342 (NEUZIL) * Column 2, line 50 - column 3, line 9; claims *	1-3,5	
			TECHNICAL FIELDS SEARCHED (Int. Cl.5)
			C 07 C 7/00
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 07-06-1990	Examiner VAN GEYT J.J.A.
CATEGORY OF CITED DOCUMENTS			
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	

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